# Predictive thermal control applied to HabEx

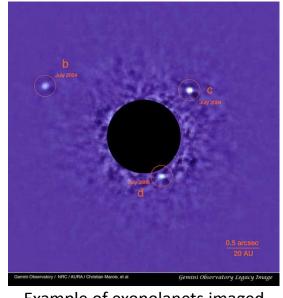
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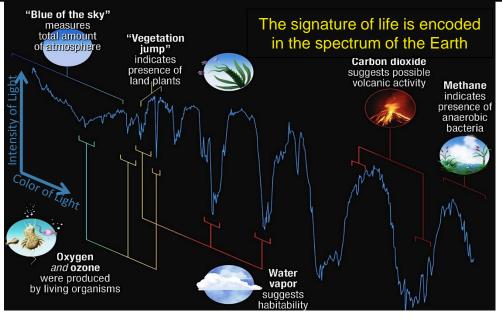
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### HabEx Brief Background

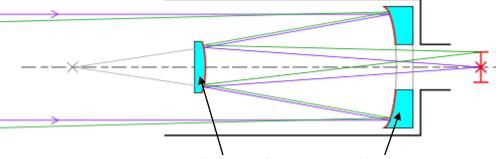




Example of exopolanets imaged with a ground based system.<sup>[1]</sup>



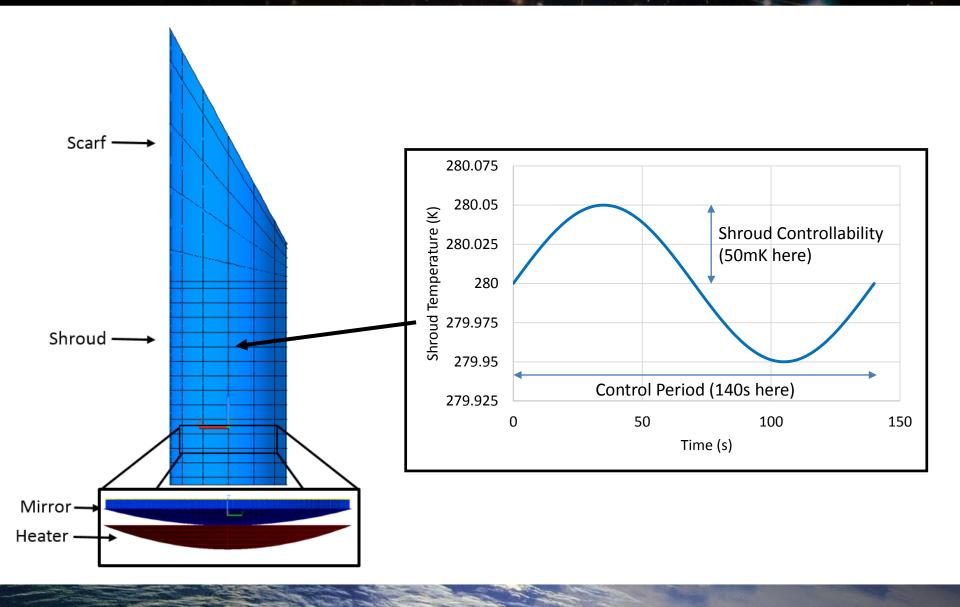
Biosignatures.<sup>[2]</sup>



SFE may not change by more than 10pm in 10 minutes Position may not move by more than ~2nm per 10 minutes

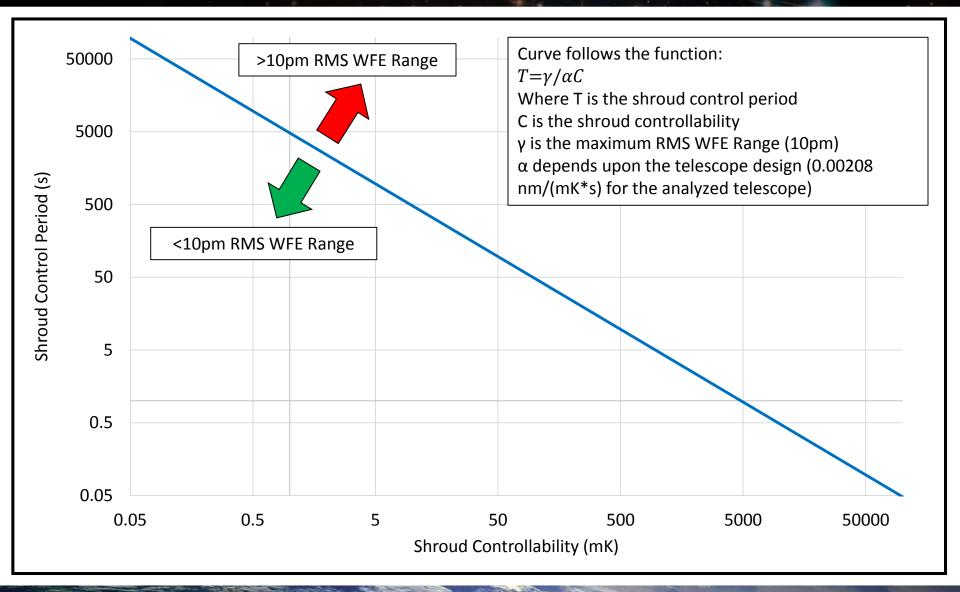
## Thermal Analysis Approach





#### Thermal Stability Requirement





#### 1-D Rod Closed-Form Model



Rod with a mass, specific heat, thermal energy, temperature and coefficient of thermal expansion of m, c<sub>p</sub>, Q, T, and CTE respectfully

Length of rod, L

 Equation 1 describes heat storage in the rod

 $Q = \rho V c_p T$  Equation 1

- Equation 3 describes linear thermal expansion
- $\frac{dQ}{dt} = \rho V c_p \frac{dT}{dt}$  Equation 2
- Algebra and calculus then Equation 5
- $(CTE)L\Delta T = \Delta L$  Equation 3

 Equation 5 shows variables that affect thermal strain rate

 $\frac{dT}{dt}(\text{CTE})L = \frac{dL}{dt} \quad \text{Equation 4}$ 

Geometry dependent: L, V, dQ/dt (surface area)

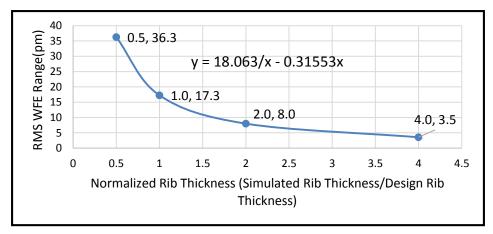
 $\frac{dL}{dt} = \frac{(\text{CTE})L}{\rho V c_n} \frac{dQ}{dt}$  Equation 5

Material dependent: CTE, ρ, c<sub>p</sub>, and dQ/dt (emissivity and absorptivity)

#### Passive Design Figures of Merit



 Numerical and analytical models agree that heat capacity and CTE have very strong affects on thermal deformation rates.



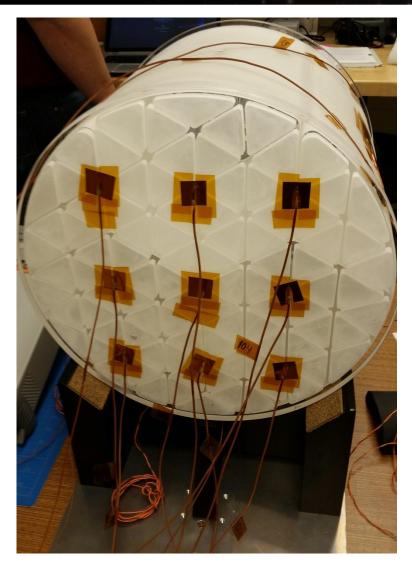
$$\frac{dL}{dt} = \frac{(\text{CTE})L}{\rho V c_p} \frac{dQ}{dt}$$

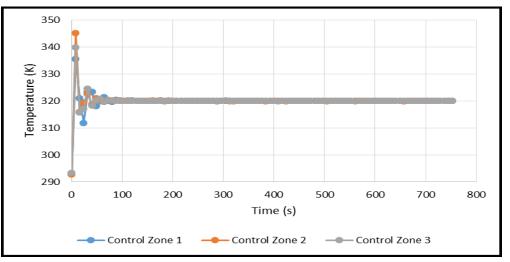
• For an actively controlled substrate, the following figures of merit are proposed:

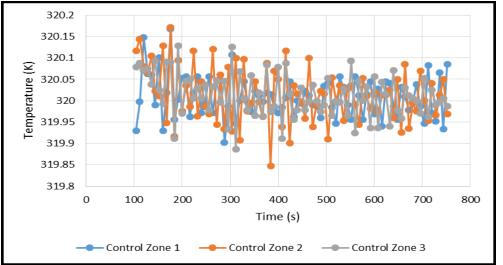
Massive Active Optothermal Stability, MAOS = 
$$\frac{\rho c_p}{CTE}$$
  
Active Optothermal Stability, AOS =  $\frac{c_p}{CTE}$ 

# Subscale Test



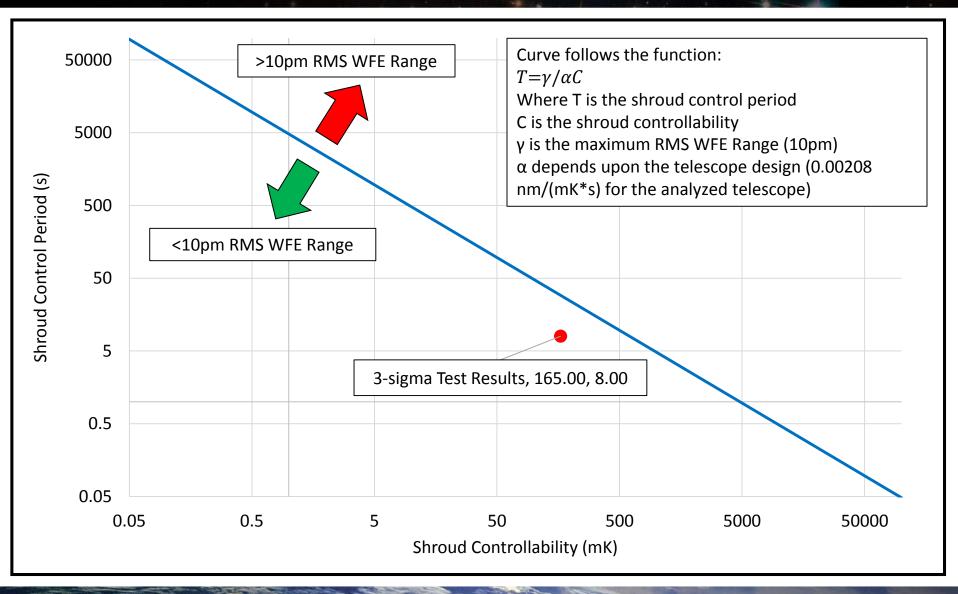






#### Test Compared to Requirement





#### Questions or Comments?



#### **Contact Information**

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